Smart Three-Dimensional Gas Chromatography

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ABSTRACT: We developed a complete computer-controlled smart 3-dimensional gas chromatography (3-D GC) system with an automation algorithm. This smart 3-D GC architecture enabled independent optimization of and control over each dimension of separation and allowed for much longer separation time for the second- and third-dimensional columns than the conventional comprehensive 3-D GC could normally achieve. Therefore, it can potentially be employed to construct a novel GC system that exploits the multidimensional separation capability to a greater extent. In this Article, we introduced the smart 3-D GC concept, described its operation, and demonstrated its feasibility by separating 22 vapor analytes.

Gas chromatography (GC) is one of the most effective methods for volatile organic compounds (VOCs) analysis and has been used in a broad range of applications. In order to further enhance the GC peak capacity, multidimensional GC is proposed and developed where each analyte is subject to multiple separations in multiple columns.1,2 In particular, comprehensive 2-dimensional GC (GC×GC) has been under intensive development in recent years. A typical GC×GC configuration has two separation columns connected in series with a thermal modulator installed in between.2,3 The modulator slices each single effluent peak from the first-dimensional (1D) column into a series of smaller segments (usually on the order of sub- to several seconds) and sends them sequentially into the second-dimensional (2D) column. Despite its enhanced separation capability, the conventional GC×GC suffers severely from the conflicting requirement for a long 2D separation time needed for sufficient 2D separation and a short modulation cycle needed for better reconstruction of the 1D separation. Usually, the 2D column is short in order to avoid the potential wrap-around issue.4 As such, the actual GC×GC peak capacity is far from the theoretical maximum n1 × n2, where n1 and n2 are the peak capacities of the 1D and 2D columns under optimal standalone conditions, respectively.1–8

In addition to GC×GC, comprehensive 3-dimensional gas chromatography (GC×GC×GC) has also been explored on the basis of the architecture similar to that in GC×GC.9–11 However, due to the aforementioned conflicting requirement, restrictions on the separation in the later stage become more stringent and detrimental. For example, while the maximally allowed 2D separation was 5 s, only 0.2 s was allowed in the 3D separation,10,11 significantly limiting the capability of GC×GC×GC.

We recently demonstrated smart multichannel 2-dimensional GC (2-D GC) architecture consisting of a flow-through on-column vapor detector and a flow routing module placed between 1D and 2D columns, which allows for much longer 2D separation time without concern of the wrap-around issue in the conventional GC×GC.12,13 The 1D and 2D retention times are directly measured by the 1D and 2D vapor detectors installed right after the corresponding columns. Through this GC architecture, the separation processes in the two adjacent dimensions are “de-coupled” and can be optimized independently to fully exploit the multiplication of the peak capacity of each dimension. Furthermore, the architecture can be conveniently cascaded for higher dimensional separation.

In this Article, we aimed to capitalize on our previous work on the smart 2-D GC and develop smart 3-dimensional GC (3-D GC) architecture. A general configuration of the proposed multichannel 3-D GC system is illustrated in Figure 1A. The system consists of three sets of columns of different polarities representing three dimensions of separation. After each column, there is a flow-through on-column nondestructive vapor detector that can detect analytes without interference to analytes or flow.14–16 Between two neighboring dimensions, a flow routing module is installed to stop/continue the flow when needed and distribute the eluted analytes into different channels of the same dimension. The overall operation procedures are described as follows. The initial vapor mixture is first separated by the 1D column into multiple peaks (clusters), each of which may contain multiple coeluted

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analytes. When the entire peak is detected, it is loaded onto the thermal injector and injected into the downstream column for higher-dimensional separation. Multiple channels in each dimension are employed to accommodate multiple peaks coming from the upstream columns. In the present work, we implemented the above smart 3-D GC concept in a 1 × 1 × 1-channel fashion (see Figure 1B). We first built a complete computer-controlled 3-D GC system with an automation algorithm and then demonstrated its feasibility by analyzing 22 analytes.

**EXPERIMENTAL SECTION**

**Materials.** All the analytes used in the experiment were purchased from Sigma (St. Louis, MO) or Fisher Scientific (Pittsburgh, PA) and had purity greater than 97%. Rxi guard column (part no. 10029, i.d. = 250 μm), Rtx-1 (part no. 10123, i.d. = 250 μm), and Rtx-5 (part no. 12623, i.d. = 250 μm) were purchased from Restek (Bellefonte, PA). SUPELCO-WAX-10 capillary column and Carbopack B adsorbent were purchased from Supelco (Bellefonte, PA). Universal quick seal column connectors (part no. 23627) and universal angled “Y” connectors (part no. 20403-261) were purchased from Sigma and Restek, respectively. Three-port valves (part no. 009-0269-900) and mini-diaphragm pumps (part no. D713-22-01) were purchased from Parker (Cleveland, OH). All materials were used as received.

**Experimental Setup.** The schematic of the smart 3-D GC is illustrated in Figure 1B. The main function block of the system consisted of a commercial GC injector, one 0.8 m long Rtx-5 ms 1D column with the 1D flow-through on-column optical vapor detector installed at its end, one 1.0 m long Rtx-1 2D column with the corresponding 2D vapor detector, and one 3.0 m long SUPELCO-WAX-10 3D column with the corresponding 3D vapor detector. The flow routing module between the two adjacent separations consisted of one three-port valve and one thermal injector. The details of the vapor detector, the three-port valve, and the thermal injector can be found in the Supporting Information.

The column polarity for each individual dimension was similar to what had been reported previously. The 1D column was intermediate polar Rtx-5 ms. In the latter two dimensions, we adopted the conventional column selection in GC×GC systems to reach a high degree of “orthogonality.” Therefore, nonpolar Rtx-1 and polar SUPELCO-WAX-10 were chosen for the 2D and 3D columns, respectively. In order to fully demonstrate the advantages of the 3-D GC system while using the limited collections of testing analytes that we had, in this 1 × 1 × 1 3-D GC setup, we intentionally shortened the length of the 1D and 2D columns to limit their maximum separation capabilities so that the benefit of the 3-D separation could become more evident in the upcoming tests.

The analysis was conducted in an isothermal condition at room temperature. The analytes were prepared and mixed in a cleansed container and then sampled by a solid-phase microextraction (SPME) sampler and quickly injected into a Varian 3000 GC injector preheated to 250 °C. The head pressure of the GC injector was set to zero. Gas analytes and ultrahigh purity (UHP) helium (used as carrier gas) were drawn into the system by the mini-diaphragm pump at a flow rate of approximately 6.5 mL/min. The entire operation was controlled by a computer with an in-house automation algorithm which controls the switching of valves based on peak detection from sensors adapted from our 2-D GC operation algorithm reported previously.

**Operation Procedures.** Initially, all the columns were connected via the three-port valves. The analytes were injected through a GC injector. Then, the operation procedures consisted of three steps (Figure 2).

**Step 1.** The analytes underwent the 1D separation. When an eluted peak, which might contain multiple coeluted analytes, passed the 1D detector and was trapped by the first thermal injector, a control signal was sent to the first three-port valve to disconnect the 1D and 2D columns so that the subsequent separation in the 1D column was suspended. Meanwhile, the...
first thermal injector was turned on to reach up to 300 °C to inject the trapped analytes into the 2D column.

**Step 2.** This step is essentially the same as Step 1. The analytes underwent the 2D separation. When an eluted peak, which might contain multiple coeluted analytes, passed the 2D detector and was trapped by the second thermal injector, a control signal was sent to the second three-port valve to disconnect the 2D and 3D columns so that the subsequent separation in the 2D column was suspended (Note that the separation in the 1D column was still suspended). Meanwhile, the second thermal injector was turned on to reach up to 300 °C to inject the trapped analytes into the 3D column.

**Step 3.** The analytes underwent the 3D separation. When all the analytes under the 3D separation were eluted or after a preset time interval (e.g., 5 min), the second three-port valve was reconnected to resume the 2D separation, and the subsequently eluted peaks from the 3D column were injected into the 1D column according to Step 2. When all the analytes under the 2D separation were eluted or after a preset time interval, the first three-port valve was reconnected to resume the 1D separation according to Step 1.

### RESULTS AND DISCUSSION

Figure 3 illustrates the details of how the smart 3-D GC system works by using four analytes, ethylene glycol monoethyl ether, chlorobenzene, ethylene glycol monomethyl ether, and isopropanol (Analyte #17−#20 in Table 1), as a model system. These four analytes were coeluted from the 1D column, as represented by a single peak in the lower trace of Figure 3. After the entire peak was detected, it was injected into the 2D column at 768 s (Arrow 1 in Figure 3). The 2D separation yielded two coeluted peaks with the first peak containing Analyte #17 and #18 and the second peak containing Analyte #19 and #20. At 808 s (Arrow 2), the first peak from the 2D column was injected into the 3D column, and meanwhile, the 3D separation was suspended. The 3D separation resulted in two well-resolved peaks representing Analyte #17 and #18, respectively. At 955 s (Arrow 3), the 3D separation was complete and the 3D separation was resumed. Then, the second peak was eluted out of the 3D column, and at 992 s (Arrow 4), this peak was injected into the 3D column, which resulted in two well-resolved peaks representing Analyte #19 and #20, respectively.

**Analysis of 22 VOCs.** After the illustration of the working principle of the smart 3-D GC system, we demonstrated complete separation of 22 analytes listed in Table 1. To highlight the capability of the smart 3-D GC, these analytes were intentionally selected so that some of them were coeluted at the 1D and 2D separation. As shown in Figure 4, after the 1D separation, 5 coeluted peaks emerged, which were further separated into 9 coeluted peaks after the 2D separation. Eventually, all analytes were separated after the 3D separation.

**Retention Time Calculation and Chromatogram Construction.** Each analyte undergoing this 3-D GC system has three retention times ($t_{\text{start}}$, $t_{\text{resume}}$, and $t_{\text{suspend}}$) corresponding to three-dimensional separation, which can easily be extracted on the basis of the real-time chromatogram traces in Figure 4 using the following equation:

$$t_R = t_{\text{elute}} - \sum t_{\text{suspend}} + \sum t_{\text{resume}} - t_{\text{start}}$$

where $t_{\text{start}}$ and $t_{\text{elute}}$ are the time when analytes are injected and eluted out of a particular column, respectively. $t_{\text{suspend}}$ and $t_{\text{resume}}$ are the time when the separation is suspended and resumed, respectively. For example, to calculate the 2D retention time of ethylene glycol monomethyl ether (Analyte #19) shown in Figure 3, we used $t_{\text{start}} = 768$ s, $t_{\text{suspend}} = 808$ s, $t_{\text{resume}} = 955$ s, and $t_{\text{elute}} = 984$ s to obtain $t_{R,2D} = 69$ s. Similarly, using $t_{\text{start}} = 992$ s and $t_{\text{elute}} = 1102$ s, we obtain $t_{R,3D} = 110$ s for #19. Note that no separation suspension or resumption was conducted for the 3D separation for #19. Therefore, $t_{\text{suspend}} = t_{\text{resume}} = 0$ s.

### Table 1. Analytes Used in the Experiment

<table>
<thead>
<tr>
<th>Analyte</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>carbon disulfide</td>
</tr>
<tr>
<td>2</td>
<td>dichloroethylene</td>
</tr>
<tr>
<td>3</td>
<td>methyl t-butyl ether</td>
</tr>
<tr>
<td>4</td>
<td>dichloromethane</td>
</tr>
<tr>
<td>5</td>
<td>chloroform</td>
</tr>
<tr>
<td>6</td>
<td>hexane</td>
</tr>
<tr>
<td>7</td>
<td>dimethylformamide</td>
</tr>
<tr>
<td>8</td>
<td>benzene</td>
</tr>
<tr>
<td>9</td>
<td>carbon tetrachloride</td>
</tr>
<tr>
<td>10</td>
<td>trichloroethylene</td>
</tr>
<tr>
<td>11</td>
<td>dioxane</td>
</tr>
<tr>
<td>12</td>
<td>toluene</td>
</tr>
<tr>
<td>13</td>
<td>vinyl acetate</td>
</tr>
<tr>
<td>14</td>
<td>tetrachloroethylene</td>
</tr>
<tr>
<td>15</td>
<td>ethylbenzene</td>
</tr>
<tr>
<td>16</td>
<td>ethylene glycol</td>
</tr>
<tr>
<td>17</td>
<td>ethylene glycol monomethyl ether</td>
</tr>
<tr>
<td>18</td>
<td>chlorobenzene</td>
</tr>
<tr>
<td>19</td>
<td>ethylene glycol mono-ethyl ether</td>
</tr>
<tr>
<td>20</td>
<td>isopropanol</td>
</tr>
<tr>
<td>21</td>
<td>styrene</td>
</tr>
<tr>
<td>22</td>
<td>m-xylene</td>
</tr>
</tbody>
</table>
With all 3-D retention times acquired, it is then straightforward to construct the 3-D chromatogram as shown in Figure 5A. A 2-D chromatogram can easily be formed by projecting the 3-D chromatogram onto any 2-D space, as exemplified in Figure 5B. Note that over 100 s of 1D and 2D separation was used in our 3-D GC system to separate those 22 analytes, which was otherwise very difficult to accomplish with the conventional GC×GC or GC×GC×GC architecture. Note that, due to the additive (or scalable) nature of the smart GC architecture, the above 3-D GC system can also be interpreted as a “pre-separation” stage (i.e., the 1D separation), followed by a smart 2-D GC subsystem. With this “pre-separation” stage, analytes are regrouped before entering the 2-D GC subsystem and each group may contain far fewer analytes than originally in the vapor mixture, which can significantly lessen the separation burden on the downstream 2-D GC subsystem and improve its performance.

**CONCLUSION AND FUTURE WORK**

We have built a complete smart 3-D GC system that allows for independent control over each dimension of separation and much longer separation time for higher dimensions, thus providing a platform for us to fully exploit the power of the multidimensional GC. Future work will be to adapt the smart 3-D GC to develop smart 3-D micro-GC where multidimensional separation provides the much needed high peak capacity. Multiple channels will also be implemented to shorten the overall analysis time. In addition, a hybrid system, which was previously demonstrated in a different configuration, will be explored that includes a “pre-separation” stage and a conventional GC×GC (or micro-GC×GC) subsystem. Furthermore, the temperature ramping method can be implemented to expedite the analysis time, as shown in our previous work. Finally, we note that our current demonstration required baseline separation in each column so that the algorithm was able to decide a peak. In practice, baseline separation may not be achieved. A possible solution may be a “cut and stitch” method that involves multiple columns in the same dimension. Another possible solution may be to treat the 1D separation as the sample preparation stage as discussed earlier. Complex samples will be preseparated into simpler groups, each of which will then be subjected to 2-D separation. In the future, this issue needs to be addressed before the proposed smart 3-D GC becomes practically useful.
ASSOCIATED CONTENT

Supporting Information
Additional information as noted in the text. This material is available free of charge via the Internet at http://pubs.acs.org.

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Notes
The authors declare no competing financial interest.

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